

GNSS CALIBRATION REPORT

G1G2_1020_2023

Prepared by: Florian Heimbach (PTB)
Time Dissemination
Working Group

Approved by: Juergen Becker (PTB)
Time Dissemination
Working Group

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REFERENCES

| REFERENCES | |
|-------------|---|
| RD01 | 2020 Group 1 GNSS calibration trip (CAL_ID 1001-2020) |
| RD02 | BIPM guidelines for GNSS calibration, V3.0, 02/04/2015 |
| RD03 | BIPM Procedure for computing raw difference of GNSS code measurements for geodetic receivers, dclrinex software version 3.1, April 2021 |
| RD04 | J. Kouba, P. Heroux, 2002, "Precise Point Positioning Using IGS Orbit and Clock Products", GPS Solutions, Vol. 5, No. 2, 12-28 |
| RD05 | W. Lewandowski, C. Thomas, 1991, "GPS Time transfers," Proc. IEEE, Vol. 79, No. 7, 991-1000 |
| RD06 | P. Defraigne and G. Petit, "CGGTTS-Version 2E: an extended standard for GNSS time transfer", Metrologia 52 (2015) G1 |
| RD07 | D. A. Howe and N. Schlossberger, "Characterizing Frequency Stability Measurements Having Multiple Data Gaps", IEEE Transactions on Ultrasonics, Ferroelectrics, and Frequency Control, Vol. 69, No. 2 (2022) |
| RD08 | BIPM Template for calibration report to the BIPM, V3.1, 29/08/2015 |

ACRONYMS

| ACRONYMS | |
|-----------------|---|
| BIPM | Bureau International des Poids et Mesures, Sèvres, France |
| CAB DLY | Antenna Cable Delay |
| CGGTTS | CCTF Generic GNSS Time Transfer Standard |
| DCLRINEX | Differential calibration software using the pseudoranges directly read from the RINEX files, software was provided by the BIPM |
| EURAMET | The European Association of National Metrology Institutes |
| FMTC | Center for Physical Sciences and Technology, Lithuania |
| IGS | International GNSS Service |
| INT DLY | Internal Signal Delay |
| GNSS | Global Navigation Satellite System |
| PPP | Precise Point Positioning |
| PTB | Physikalisch-Technische Bundesanstalt, Braunschweig, Germany |
| REF DLY | Reference Delay |
| RINEX | Receiver Independent Exchange Format |
| R2CGGTTS | RINEX-to CGGTTS conversion software, provided by ORB / BIPM |
| TDEV | Time Deviation |
| TIC | Time Interval Counter |

EXECUTIVE SUMMARY

As part of the support of the BIPM Time and Frequency Group by EURAMET G1 laboratories, PTB conducted a relative calibration of GNSS equipment of FMTC, Lithuania, with respect to the calibration of PTB receiver PT13, which currently serves as the reference receiver in all GNSS time links to PTB in the context of realization of TAI. The PT13 signal delays for GPS and Galileo were determined by BIPM as reported with CAL_ID 1001-2020 [RD01]. PTB provided its receiver PTBM for the purpose as traveling equipment. The current campaign followed as much as possible the BIPM Guide [RD02] and results will be reported using CAL_ID 1020-2023. Results provided are the visited receiver's internal delays for GPS P-code signals on the two frequencies L1 and L2 (INT DLY (P1), and INT DLY(P2)) and the C/A-code signal on L1 (L1C). The delays were determined using the DCLRINEX software, which was provided by the BIPM [RD03].

This report documents the installation, data taking and evaluation during the campaign. Its structured based on the BIPM template [RD08].

The determination of the internal delay values of the receiver at the visited site is a three-step process.

At first (Common-Clock 1, CC1), the traveling receiver, PTBM, was compared to the "golden" receiver, PT13, and the offset between the actual and the assumed PTBM delay values were determined.

After that, the receiver was installed at the visited site. At FTMC, two GNSS receivers are reported to BIPM, named LT02 and LT03. These are connected to different time sources, of which one is defined as the local UTC. PTBM was first connected to the same clock as the receiver LT03 and operated for a week. After this week, PTBM was operated while being connected to the second clock, which is time source for the receiver LT02. With these measurements, the internal delay values of the devices under test and their statistical properties were determined with respect to PTBM.

Finally, the stability of the PTBM delays was assessed by a second Common-Clock measurement (CC2) in PTB. Based thereon, the "final" INT DLY values of the visited receivers and their uncertainty values were calculated.

The structure of this report follows this sequence of work. After presentation of the participants and schedule, a general section follows that contains the (mathematical) calibration procedure, followed by a report of data collection at PTB and FTMC. The final results and the uncertainty discussion close the report. In the Annex the BIPM information tables are reproduced.

The final results are included in Table 5-1. The internal GPS delays of receivers LT02 and LT03 were determined with an uncertainty of 1.3 ns for dual frequency observations.

As a reminder: All uncertainty values reported in this document are 1- σ values.

The responsible party at PTB quality management gave the advice to stress in this report that the correctness of all results and of the stated uncertainty values relies partially on the correctness of the entries in the installation report (BIPM information tables) provided by the visited institute.

1. DESCRIPTION OF EQUIPMENT AND OPERATIONS

1.1. PARTICIPANTS

Table 1-1 List of participants

| Institute | Point of contact | Site address |
|-----------|---|--|
| PTB | Florian Heimbach 0049 531 592 4422 florian.heimbach@ptb.de | PTB, AG 4.42 Bundesallee 100 38116 Braunschweig, Germany |
| FTMC | Rimantas Miškinis 00370 687 80333 Rimantas.miskinis@ftmc.lt | FMTC Center for Physical Sciences and Technology Saletekio av. 3 LT-10257 Vilnius, Lithuania |

1.2. TRAVELING EQUIPMENT

The PTBM traveling measurement set-up consists of a 19"-chassis, containing a GNSS receiver (Septentrio PolaRx5TR), a TIC (Piktime T4100U) and internal cabling. The auto compensation mode of the GNSS receiver was set to "ON" during the whole calibration trip. The set-up further includes an antenna (Navexperience 3G+C REFERENCE), 25 meters LMR-400 antenna cable, an N to TNC adapter and a laptop.

The delay from the visited UTC reference point to the calibration reference point was measured by a SI SR620 TIC (SN: 4832). The measurement was carried out by staff from FTMC, who also provided the TIC.

1.3. VISITED EQUIPMENT

Table 1-2 List of the visited equipment

| Institute | Status of equipment | Dates of measurement | Receiver type | BIPM code | RINEX name |
|-----------|---------------------|-------------------------|---------------|-----------|------------|
| FTMC | Group 2 | 28.11.2023 - 03.12.2023 | TTS-5 | LT03 | LT03 |
| FTMC | Group 2 | 04.12.2023 - 08.12.2023 | TTS-5 | LT02 | LT02 |

1.4. SCHEDULE

Table 1-3 Schedule of the campaign

| Date | Institute | Action | Remarks |
|--------------------------------|-----------|--|--|
| 2023-11-01 until 2023-11-07 | PTB | First common-clock comparison between PTBM and PT13 | 7 days used for the evaluation, MJD 60249 - 60255 |
| 2023-11-28 until 2023-12-03 | FTMC | Operation of PTBM in parallel with local receiver LT03 | 6 days used for the evaluation, MJD 60276 - 60281 |
| 2023-12-04 until 2023-12-08 | FTMC | Operation of PTBM in parallel with local receiver LT02 | 4 days used for the evaluation, MJD 60282 - 60286 |
| 2023-12-15 until 2023-12-21 | PTB | Operation of PTBM after return | 7 days used for the evaluation, MJD 60659 - 60665 |

1.5. CALIBRATION PROCEDURE

When dealing with G1G2 calibrations, in principle we distinguish receivers V, T, and G: V for visited, T for traveling, and G for golden reference.

G1 labs have committed to ship their T to the other sites. In the current campaign, PT13 (named PTBB when referred to as IGS station) serves as the reference receiver G. The PT13 signal delays for GPS and Galileo were determined by BIPM as reported with CAL_ID 1001-2020 [RD01]. PTBM served as the traveling receiver T.

Conventionally, the receiver delay D is considered as the sum of different terms that are defined subsequently:

(1) INT DLY

The internal signal delay represents the sum of $X_R + X_S$.

X_R represents the receiver hardware delay, between a reference point whose definition depends on the receiver type and the internal time reference of the measurements. X_S represents the antenna delay, between the phase center and the antenna cable connector at the antenna body. We distinguish the two quantities for the two frequencies, f_1 and f_2 .

INT DLY(f_1) and INT DLY(f_2) of receiver V are the basic quantities that are determined during the relative calibration. For calculating ionosphere-free observation data, INT DLY(f_3) is calculated as $2.54 \times \text{INT DLY}(f_1) - 1.54 \times \text{INT DLY}(f_2)$ for GPS, and as $2.26 \times \text{INT DLY}(f_1) - 1.26 \times \text{INT DLY}(f_2)$ for Galileo, respectively. In figures and results tables, we use the designation P1, P2 for GPS, and E1, E5a for Galileo, instead of f_1 , f_2 .

The following terms are considered frequency independent, i.e. no distinction is made for f_1 and f_2 .

(2) CAB DLY

The sum $X_C + X_D$ represents the antenna cable delay (CAB DLY).

X_C corresponds to the delay of the long cable from the antenna to the input connector at either the antenna splitter or the receiver body directly. If a splitter is installed, X_D corresponds to the delay of the splitter and the small cable up to the receiver body. For a simple set-up with just an antenna cable, $X_D = 0$.

(3) REF DLY

The sum $X_P + X_O$ represents the reference delay (REF DLY).

X_P corresponds to the delay of the cable between the laboratory reference point for local UTC and the 1 PPS-in connector of the receiver.

X_O corresponds to the delay between the 1PPS-in connector and the receiver internal reference point, the latter depending on the receiver type:

- For Septentrio PolaRx4: X_O available at the 1 PPS-out socket of the receiver
- For Septentrio PolaRx5TR: optionally X_O is determined autonomously by the receiver, or it can be determined alike to the PolaRx4.
- For DICOM GTR50, GTR51 and GTR55: $X_O = 0$,
- For TTS-4: RD02, Section 2.3.2, and Annex G specify the procedure for TTS-4, which in detail depends on the software version.

PT13 (PolaRx5TR) has been installed in April 2019, and the PPS IN Delay Compensation option has never been used. On the contrary, PTBM (PolaRx5TR) normally makes use of the auto-compensation option as it reduces the number of measurements and potential errors at the visited site. In this case, the REF DLY is the offset between the UTC(k) reference point and the input to the PPS IN socket on the PTBM rack.

For clarity, Figure 1-1 shows the traveling equipment in two views and screenshots of the PPS configuration menu of the PolaRx5 RxControl software and the receiver message received when the auto-compensation is active.

The distinction of the individual components of the receiver delay reflects the fact that two of them, 2 and 3, can in principle be measured with standard laboratory equipment. Changes of the receiver installation typically affect cabling and thus such delays.

The quantity to be determined by the relative calibration is the INT DLY. The INT DLY of the device under test is determined in such a way that the common-clock differences obtained between the device under test and the reference are zero on average. The INT DLY of T may need to be adjusted so that T and G match, but in practice the small correction to be applied is considered only when INT DLY of V is adjusted to G, using T as intermediate for the measurements made at the different sites.

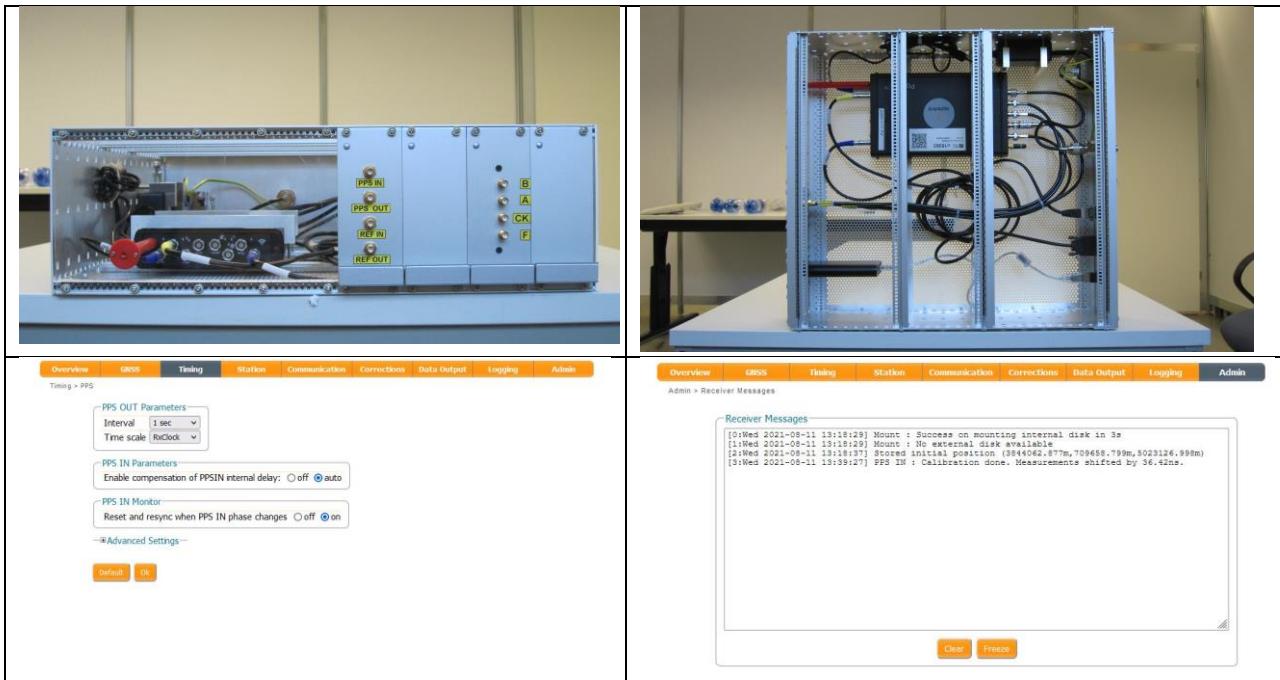


Figure 1-1 PTBM: views of the device and RxControl configuration and messages regarding PPS In and OUT.

2. DATA USED

The G, T, and V receivers are all GNSS geodetic receivers and provide RINEX observation files. RINEX navigation files produced by the PT13 receiver were used for CC1 and CC2 analysis. RINEX navigation files from PTBM were used at all stages. Code measurements were taken from the pseudoranges directly read from the RINEX files by the software DCLRINEX dedicated to differential calibration, as provide by BIPM [RD03]. The software produces raw code differences of co-located receivers from the pseudoranges as

$$\text{RAW DIF}_{T-G}(f) = \text{TOT DLY}_T(f) - \text{TOT DLY}_G(f), \quad (1)$$

with $\text{TOT DLY}_R(f)$ and $\text{TOT DLY}_T(f)$ representing the total delays of the reference and traveling receiver respectively. The total delay of G, or T can be written as

$$\text{TOT DLY}(f) = \text{INT DLY}(f) + \text{CAB DLY} - \text{REF DLY}. \quad (2)$$

This report states the differences in system delays $\Delta\text{SYS DLY}$ according to [RD08]. The system delay is described as the sum of the INT DLY and the CAB DLY.

$$\text{SYS DLY}(f) = \text{INT DLY}(f) + \text{CAB DLY} \quad (3)$$

The $\Delta\text{SYS DLY}$ for T-G and T-V can therefore be calculated from the raw code differences and the reference delays as

$$\Delta\text{SYS DLY}_{T-G}(f) = \text{RAW DIF}_{T-G,median}(f) + \text{REF DLY}_T - \text{REF DLY}_G \quad (4)$$

and

$$\Delta\text{SYS DLY}_{T-V}(f) = \text{RAW DIF}_{T-V,median}(f) + \text{REF DLY}_T - \text{REF DLY}_V. \quad (5)$$

For the analysis of a measurement series, the RAW DIFs of all available satellites were averaged for each epoch. From this data, the median and standard deviation were determined.

Using (4) & (5), the $\Delta\text{SYS DLY}$ for V-G can be written in the form

$$\Delta\text{SYS DLY}_{V-G}(f) = \Delta\text{SYS DLY}_{T-G}(f) - \Delta\text{SYS DLY}_{T-V}(f). \quad (6)$$

Therefore, the equation

$$\text{INT DLY}_V(f) = \text{INT DLY}_G(f) + \Delta\text{SYS DLY}_{V-G}(f) + \text{CAB DLY}_G - \text{CAB DLY}_V \quad (7)$$

can be used to calculate the INT DLY of all visited receivers.

The analysis also includes the time deviations of the measurement series. The time instability (TDEV) values were determined from the epoch-averaged timelines. If applicable, data gaps in the

timeline were filled using the algorithm developed by D. A. Howe and N. Schlossberger [RD07], before TDEV analysis.

3. RESULTS OF RAW DATA PROCESSING

3.1. OVERVIEW

The raw code differences of the pairs of co-located receivers during the data acquisition period are generated using the DCLRINEX software. The stated raw calibration results are taken as the median of the raw differences. The associated uncertainties are derived from the TDEV at 50000 s. The default value of 0.1 ns is chosen if the measured TDEV is less than 0.1 ns.

Table 3-1 Summary information on the raw calibration results for GPS signals (all values in ns)

| Pair | Date | RAWDIF(P1) | Unc. | RAWDIF(P2) | Unc. |
|------------|---------------|------------|------|------------|------|
| PTBM-PT13 | 60249 - 60255 | 59.7 | 0.1 | 60.5 | 0.1 |
| PTBM-LT02 | 60282 - 60286 | 75.2 | 0.1 | 77.7 | 0.1 |
| PTBM- LT03 | 60276 - 60281 | 76.5 | 0.1 | 66.2 | 0.1 |
| PTBM-PT13 | 60659 - 60665 | 54.9 | 0.1 | 55.5 | 0.1 |

3.2. COMMON-CLOCK SET-UP IN PTB: PERIOD 1

For CC1, PTBM was operated for 7 days at PTB. The installation of the receivers in PTB is depicted in Figure 3-1 for PPS signals and in Figure 3-2 for 5 MHz (and 10 MHz) signals.

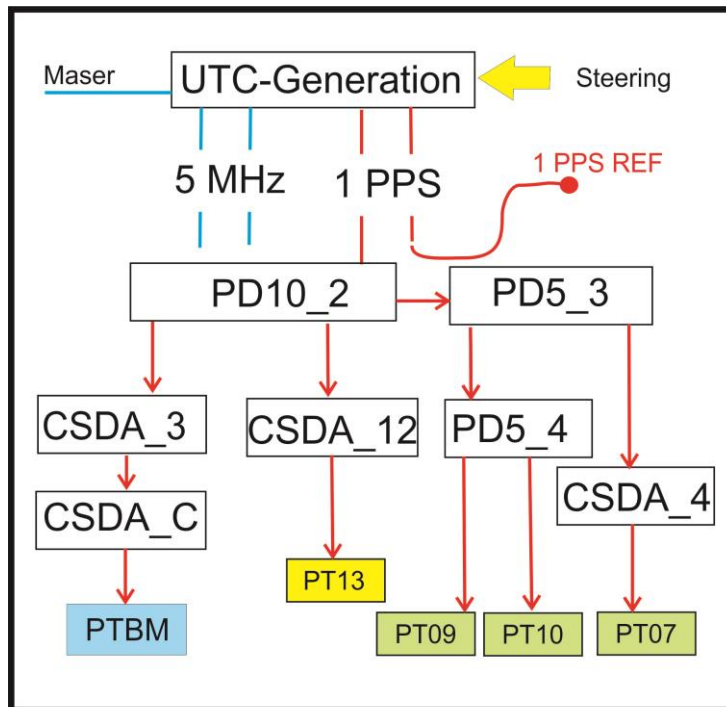


Figure 3-1 UTC(PTB) reference point and 1 PPS signal distribution to PT13, PTBM, and other receivers; PD stands for pulse distributor, CSDA stands for clock signal distribution amplifier

A clarification may be helpful regarding the 1 PPS REF point. When measuring with a TIC the time difference between Port A = UTC(PTB), and Port B = 1 PPS REF, then the result is +2.7 ns. Figure 3-3 illustrates the installation of GNSS antennas on the roof of the PTB time laboratory (clock hall) during CC1.

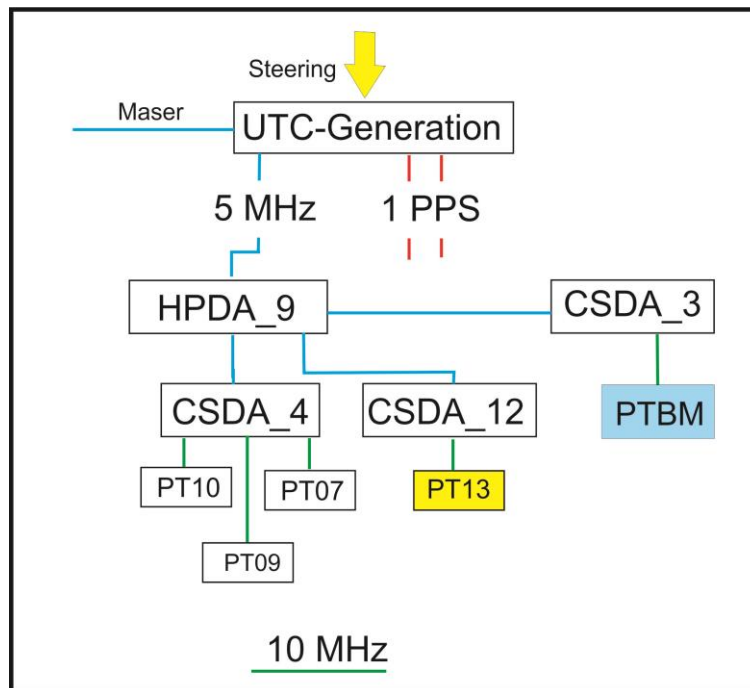


Figure 3-2 UTC(PTB) signal distribution (5 MHz, 10 MHz) to PT13, PTBM, and other receivers
HPDA stands for High-precision distribution amplifier (for rf frequencies)

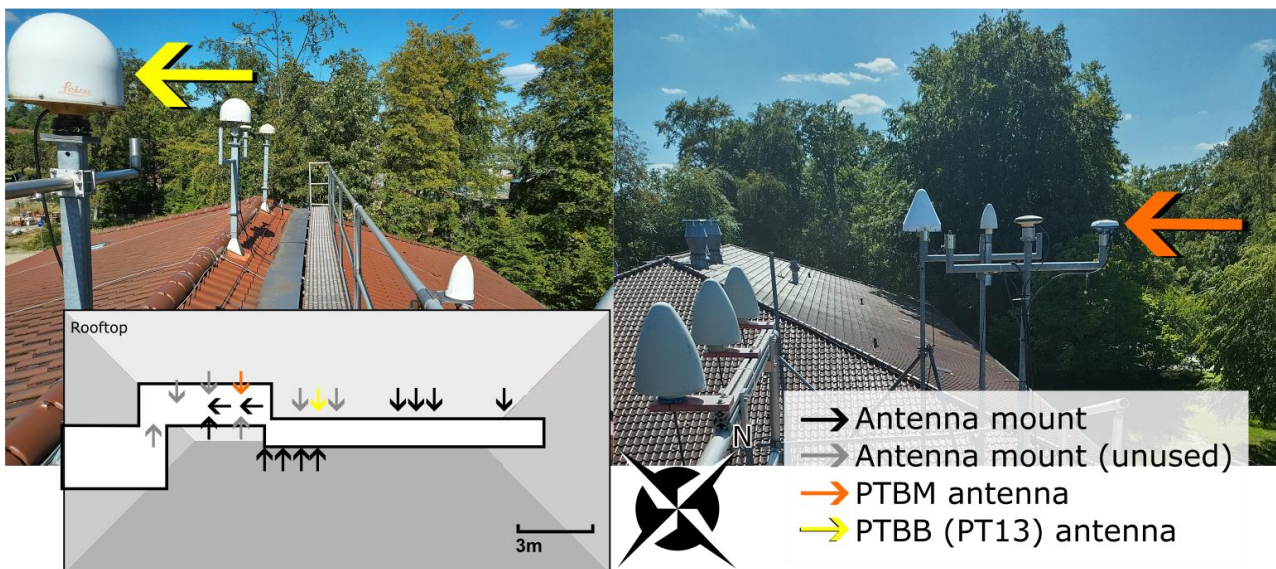


Figure 3-3 Installation of GNSS antennas at PTB, PT13 antenna (yellow) and PTBM antenna during CC1 and CC2 (orange)

The period 60249 to 60255 (7 days) was chosen to determine the initial PTBM INT DLY values (CC1). The result of comparison with PT13 as the reference are shown in Figure B-1. The figures show the raw code differences and the corresponding TDEVs. The numerical results are given in Table 3-1.

3.3. OPERATION OF PTBM AT FTMC

The PTBM was dispatched on 8th of November 2023 and set-up at FTMC on the 20th of October. PTBM was operated for 18 days. FTMC operates two GNSS receivers with designation LT02 and LT03 whose delays were determined. Information sheets about these receivers are shown in Annex A. Both are PikTime Systems TTS-5 GNSS receivers. As FTMC is operating the two receivers on two different time sources, it was decided to measure LT03 and LT02 successively.

The PPS signal distribution to PTBM and FTMC receivers is illustrated in Figure 3-4 and Figure 3-5. The antenna installation at FTMC is shown in Figure 3-5. PTBM was operated with its own antenna and antenna cable.

Raw code differences and the corresponding TDEVs are shown in Annex B starting with Figure B-2 and B-3. The numerical results are given in Table 3-1.

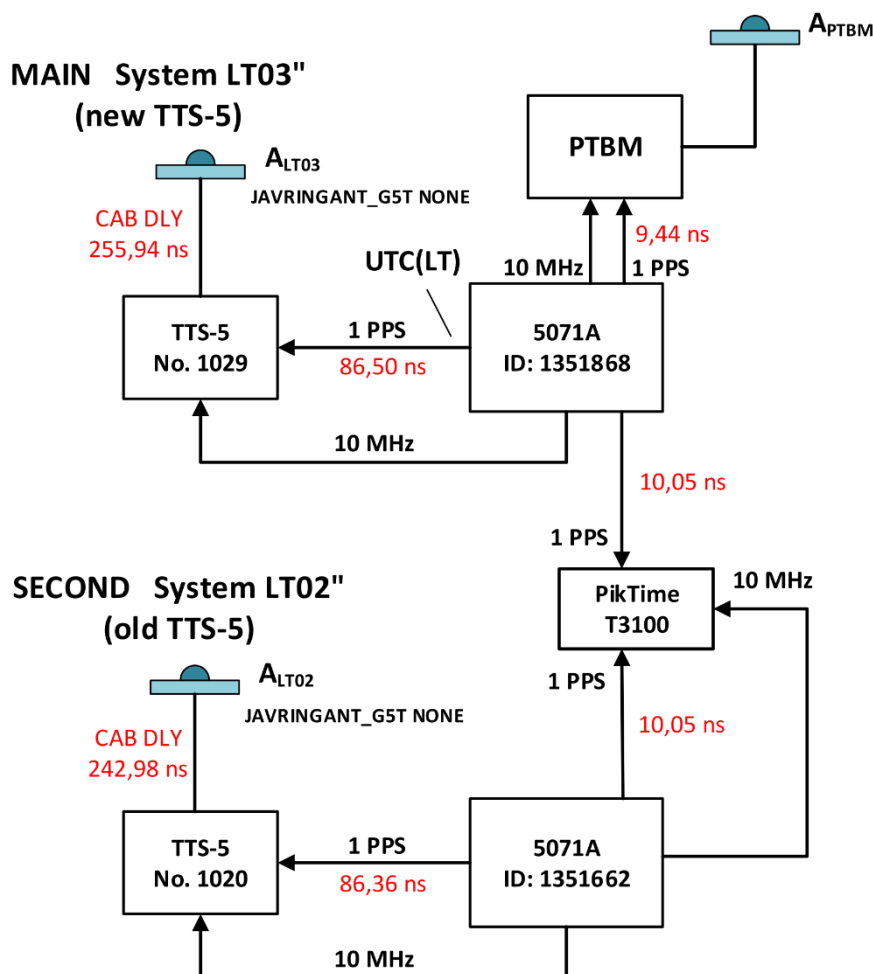


Figure 3-4 PPS signal distribution at FTMC with PTBM as operated from MJD60268 until MJD60282

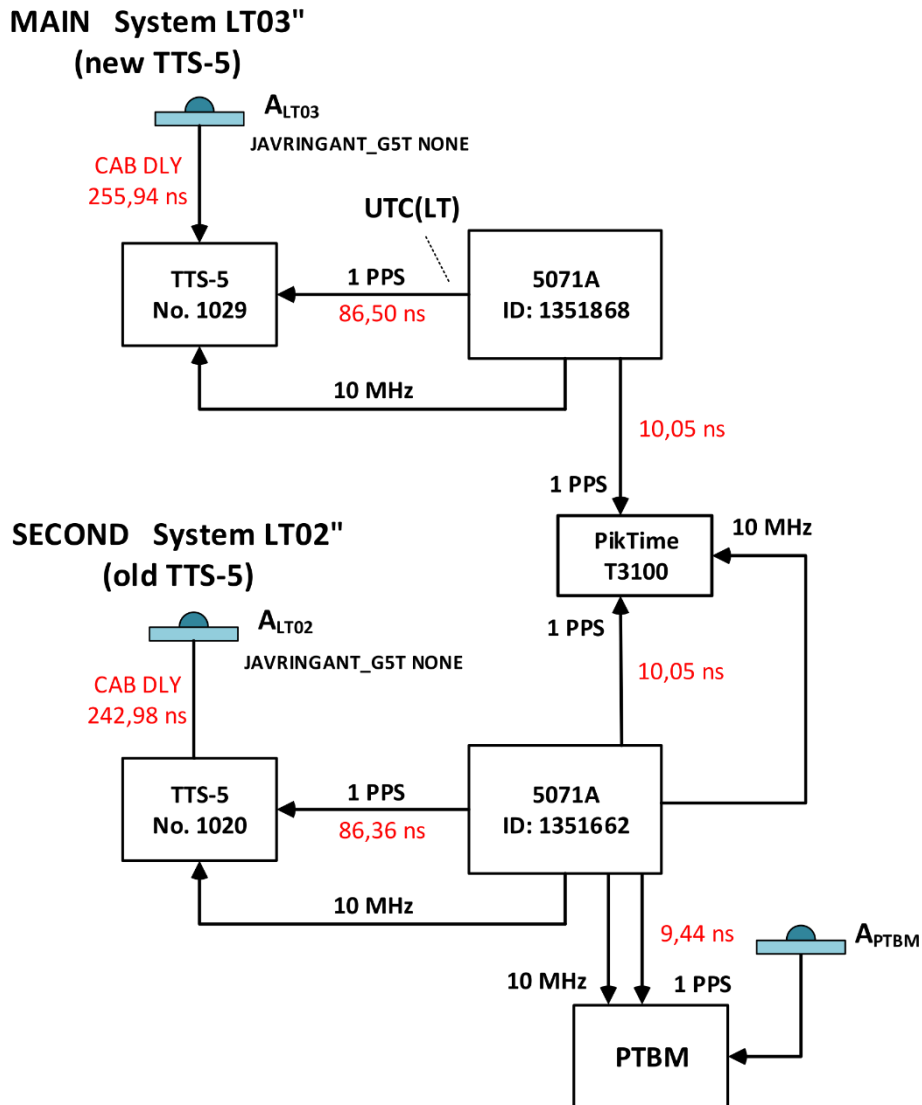


Figure 3-5 PPS signal distribution at FTMC with PTBM as operated from MJD60282 until MJD60286



Figure 3-5 PTBM antenna installation at FTMC

3.4. COMMON-CLOCK SET-UP IN PTB: PERIOD 2

The period 60659 to 60665 (7 days) was chosen to determine PTBM INT DLY values during the common clock period CC2. The configuration of PTBM was “standard”, the automatic PPS IN delay compensation was activated. The result of comparison with PT13 as the reference are shown in Figure B-4. The figures show the raw code differences and the corresponding TDEVs. The numerical results are given in Table 3-1.

4. CALIBRATION RESULTS

4.1. TRAVELING SYSTEM WITH RESPECT TO THE REFERENCE SYSTEM

Table 4-1 Calibration results T vs. G (all values in ns)

| Pair | Date | REF DLY _T | REF DLY _G | RAW DIF | Δ SYS DLY _{T-G} | Code |
|-----------|---------------|----------------------|----------------------|---------|---------------------------------|------|
| PTBM-PT13 | 60249 - 60255 | 42.8 | 56.2 | 59.7 | 46.3 | P1 |
| PTBM-PT13 | 60249 - 60255 | 42.8 | 56.2 | 60.5 | 47.1 | P2 |
| PTBM-PT13 | 60659 - 60665 | 47.5 | 56.2 | 54.9 | 46.2 | P1 |
| PTBM-PT13 | 60659 - 60665 | 47.5 | 56.2 | 55.5 | 46.7 | P2 |

4.2. TRAVELING SYSTEM WITH RESPECT TO THE VISITED SYSTEM

Table 4-2 Calibration results T vs. V (all values in ns)

| Pair | Date | REF DLY _T | REF DLY _V | RAW DIF | Δ SYS DLY _{T-V} | Code |
|-----------|---------------|----------------------|----------------------|---------|---------------------------------|------|
| PTBM-LT02 | 60282 - 60286 | 9.4 | 81.1 | 75.2 | 3.5 | P1 |
| PTBM-LT02 | 60282 - 60286 | 9.4 | 81.1 | 77.7 | 6.0 | P2 |
| PTBM-LT03 | 60276 - 60281 | 9.4 | 86.4 | 76.5 | -1.6 | P1 |
| PTBM-LT03 | 60276 - 60281 | 9.4 | 86.4 | 66.2 | -11.8 | P2 |

4.3. VISITED SYSTEM WITH RESPECT TO THE REFERENCE SYSTEM

Table 4-3 Calibration results V vs. G (all values in ns)

| Pair | Date | CAB DLY _V | CAB DLY _G | Δ SYS DLY _{V-G} | Δ INT DLY _{V-G} | Code |
|-----------|------|----------------------|----------------------|---------------------------------|---------------------------------|------|
| PT13-LT02 | 2023 | 243.0 | 205.7 | 42.7 | 5.4 | P1 |
| PT13-LT02 | 2023 | 243.0 | 205.7 | 40.9 | 3.7 | P2 |
| PT13-LT03 | 2023 | 255.9 | 205.7 | 47.9 | -2.4 | P1 |
| PT13-LT03 | 2023 | 255.9 | 205.7 | 58.8 | 8.5 | P2 |

The numerical results of the two common-clock campaigns at PTB are given in Table 4-1. The Δ SYS DLY_{T-G} values agree very well with the largest change noted between CC1 and CC2 amounting 0.07 ns for P1.

4.4. INT DLY UNCERTAINTY EVALUATION

The overall uncertainty of the INT DLY values obtained as a result of the calibration is given by

$$u_{\text{CAL}} = \sqrt{u_a^2 + u_b^2}, \quad (8)$$

with the statistical uncertainty u_a and the systematic uncertainty u_b . The statistical uncertainty is related to the instability of the common clock data collected at the visited sites and PTB, respectively. The systematic uncertainty is given by

$$u_b = \sqrt{\sum_n u_{b,n}^2}. \quad (9)$$

The contributions to the sum (9) are listed and explained subsequently. Values in column P3 are calculated according to $u(\text{P3}) = \sqrt{\{u(\text{P1})^2 + (1.54 \times u(\text{P1}-\text{P2}))^2\}}$. Uncertainties for the Galileo delays are calculated according to $\sqrt{\{u(\text{E1})^2 + (1.26 \times u(\text{E1}-\text{E5a}))^2\}}$.

Note that the uncertainty of the INT DLY values of PTB's fixed receiver PT13 (G) which served as the reference is not included.

Table 4-4 Uncertainty contributions for the calibration of receiver delays at FTMC, all values in ns

| | Uncertainty | Value f1 | Value f2 | Value f1-f2 | Value f3 | Description |
|--|-------------------|----------|----------|-------------|----------|--|
| 1 | u_a (PTB) | 0.1 | 0.1 | 0.14 | | CC measurement uncertainty at PTB, TDEV max. of the two CC campaigns |
| 2 | u_a (FTMC) | 0.1 | 0.1 | 0.14 | | CC measurement uncertainty, for the FTMC receivers |
| 3 | u_a (GPS) | 0.14 | 0.14 | 0.2 | 0.34 | |
| Result of closure measurement at PTB | | | | | | |
| 4 | $u_{b,1}$ (GPS) | 0.1 | 0.4 | 0.41 | | Misclosure, see Table 4-1 |
| Systematic components due to antenna installation | | | | | | |
| 5 | $u_{b,11}$ | 0.2 | 0.2 | 0.28 | | Multipath at PTB |
| 6 | $u_{b,12}$ | 0.2 | 0.2 | 0.28 | | Multipath at FTMC |
| Installation of PTBM and visited receivers | | | | | | |
| 7 | $u_{b,21}$ | 0.2 | 0.2 | 0 | | Connection of PTBM to UTC(PTB) (REF DLY) |
| 8 | $u_{b,22}$ | 0.2 | 0.2 | 0 | | Connection of PTBM to UTC(FTMC) (REF DLY) |
| 9 | $u_{b,23}$ | 0.2 | 0.2 | 0 | | Connection of receivers at FTMC to UTC(FTMC) (REF DEL) |
| 10 | $u_{b,24}$ | 0.1 | 0.1 | 0 | | TIC nonlinearities at PTB |
| 11 | $u_{b,25}$ | 0.1 | 0.1 | 0 | | TIC nonlinearities at FTMC |
| Antenna cable delay | | | | | | |
| 12 | $u_{b,31}$ (PTB) | 0.5 | 0.5 | 0 | | Uncertainty estimation for the PTBM CAB DLY when installed at PTB |
| 13 | $u_{b,32}$ (FTMC) | 0 | 0 | 0 | | Uncertainty estimation for the PTBM CAB DLY when installed at FTMC |
| 14 | $u_{b,33}$ (FTMC) | 0.5 | 0.5 | 0 | | Uncertainty estimation for FTMC CAB DLY values |
| 15 | $u_{b,INT}$ (GPS) | 1.06 | 1.06 | 0.57 | 1.23 | |
| 16 | $u_{CAL,0}$ (GPS) | | | | 1.3 | |

As demonstrated in Table 3-1, the three receivers at FTMC show almost the same time instability. The TDEV plots in Annex B show marginal differences, and the value of 0.1 ns is a conservative estimate anyway. Thus, a single uncertainty budget can cover all other contributions.

The uncertainty contribution $u_{b,1}$ is based on the difference between the two common clock campaigns involved which was very small for the current campaign. A conservative estimate of 0.1 ns was chosen.

At PTB, the PPS IN Delay Compensation has been initiated several times, with the PTBM receiver connected to different 10 MHz cables in sequence. Results reported agreed within 0.1 ns. Thus, when the receiver is operated in the same modus at each site the achievable uncertainty is likely the lowest. This was the case during the current campaign.

An uncertainty contribution due to potential multipath disturbance is added as $u_{b,11}$ and $u_{b,12}$. If at a given epoch in time the recorded time differences REFSYS would be biased by multipath, this might change with time due to the change in the satellite constellation geometry. [RD05] gives an estimate that has often been referred to. It was agreed at the 2017 meeting of the CCTF WG on GNSS that a 0.2 ns-uncertainty should be attributed to the multipath effect.

The uncertainties of the connection of the receivers to the local time scales ($u_{b,21}$, $u_{b,22}$, $u_{b,23}$) has been estimated 0.2 ns for all cases.

The uncertainty contributions $u_{b,24}$ and $u_{b,25}$ are related to imperfections in the TIC in conjunction with the relationship between the zero-crossings of the external reference frequency and the 1 PPS signals. This “nonlinearity” is probably caused by the internal interpolation process. By connecting the travelling TIC successively to 10 MHz, using cables of different lengths, the effect was estimated to be at most 0.1 ns if 1 PPS signals with a slew rate of approximately 0.5 V/ns are used.

The measurement of antenna cable delays causes contributions $u_{b,31}$, $u_{b,32}$ and $u_{b,33}$. During the current campaign the same PTBM cable was employed on each occasion. CAB DLY values were measured at PTB in previous campaigns, with the cable rolled out and with the cable on the spool. Each measurement was made with a differential method so that the TIC-internal error should be small anyway. All results agreed within 0.1 ns if the same PPS signal source was used but differed by up to 0.5 ns when the slew rate of the pulse was significantly different. Thus, we retain an uncertainty contribution $u_{b,31}$ of 0.5 ns. For the stationary antenna cables at FTMC we conservatively assume the same uncertainty of the delay value.

Note anyway that this uncertainty contribution $u_{b,33}$ a priori has no impact on the uncertainty of the time transfer link between PTB and the visited institute. If the stated CAB DLY for the visited fixed receiver(s) would be erroneous, this would be absorbed in the INT DLY values produced as a result of the campaign.

5. FINAL RESULTS FOR THE VISITED SYSTEMS

The results of the calibration campaign G1G2_1020_2023 are summarized in Table 5-1. INT DLY values for the golden reference receiver PT13 were determined in 2021 [RD01]. The uncertainty values are taken from Table 4-4. The final INT DLY values were calculated using equation (7) with the values listed in Table 4-1, Table 4-2 and Table 4-3.

Table 5-1 Summary of final results for GPS links, all values in ns

| Reference system | Cal_Id | Date | | INT DLY (P1) | INT DLY (P2) |
|------------------|-----------|-------|-----------------------|--------------|--------------|
| PT13 | 1001-2020 | 59303 | | 31.6 | 29.3 |
| Visited system | Cal_Id | Date | u _{CAL} (P3) | INT DLY (P1) | INT DLY (P2) |
| LT02 | 1020-2023 | 60666 | 1.1 | 37.0 | 33.0 |
| LT03 | 1020-2023 | 60666 | 1.1 | 29.2 | 37.8 |

ANNEXES

ANNEX A: BIPM INFORMATION SHEETS

ANNEX B: PLOTS OF RAW DATA AND TDEV ANALYSIS

ANNEX A: BIPM CALIBRATION INFORMATION SHEETS

First common clock measurement at PTB

| | | | | |
|---|--|--|------------------|------------|
| Laboratory: | | PTB | | |
| Date and hour of the beginning of | | 2023-11-01 00:00 UTC (MJD 60249) | | |
| Date and hour of the end of measurements: | | 2022-08-11 23:59 UTC (MJD 60256) | | |
| Information on the system | | | | |
| | Local: | Traveling: | | |
| 4-character BIPM code | PT13 | PTBM | | |
| Receiver maker and type: | PolaRx5TR (5.2.0) | PolaRx5TR (5.4.0) | | |
| Receiver serial number: | S/N 470 1292 | S/N 3048338 | | |
| 1 PPS trigger level /V: | 1 | 1 | | |
| Antenna cable maker and type: Phase stabilised cable (Y/N): | ECOFLEX15 | LMR-400 (N) | | |
| Length outside the building /m: | approx. 25 | 25 | | |
| Antenna maker and type: Antenna serial number: | LEICA AR25 726333, Calib Geo++ 18.08.2015 | Navexperience 3G+C REFERENCE S/N RE 0560 | | |
| Temperature (if stabilized) /°C | | | | |
| Measured delays / ns | | | | |
| | Local: | Traveling: | | |
| Delay from local UTC to receiver 1 PPS-in (X_P) / ns | 9.59 ± 0.1 (#) | 48.5 +/- 0.2 | | |
| Delay from 1 PPS-in to internal Reference (if different): (X_O) / ns | 46.63 ± 0.1 (#) | Determined automatically by receiver software | | |
| Antenna cable delay: (X_C) / ns | 205.7 ± 0.1 | 264.9 ± 0.5 | | |
| Splitter delay (if any): | N/A | | | |
| Data used for the generation of CGGTTS files | | | | |
| | LOCAL: | Traveling | | |
| <input type="checkbox"/> INT DLY (or X_R+X_S) (GPS) /ns: | 31.6 (P1), 29.3 (P2), 33.6 (C1) (*) | 18.9 (P1) 17.1 (P2) (****) 0.0 (C1) | | |
| <input type="checkbox"/> INT DLY (or X_R+X_S) (GALILEO) /ns: | 33.6 (E1), 33.6 (E5a) (*) | 20.8 (E1), 17.9 (E5a) (****) | | |
| <input type="checkbox"/> CAB DLY (or X_C) /ns: | 205.7 | 264.9 | | |
| <input type="checkbox"/> REF DLY (or X_P+X_O) /ns: | 56.2 | 48.5 | | |
| <input type="checkbox"/> Coordinates reference frame: | ITRF | ITRF | | |
| X /m: | +3844059.86 (***) | Mast P10 | +3844062.56 (\$) | Mast P7 |
| Y /m: | +709661.56 (***) | | +709658.49 (\$) | |
| Z /m | +5023129.87 (***) | | +5023127.88 (\$) | |
| General information | | | | |
| <input type="checkbox"/> Rise time of the local UTC pulse: | 3 ns | | | |
| <input type="checkbox"/> Is the laboratory air conditioned: | Yes | | | |
| Set temperature value and uncertainty: | 23.0 °C, peak-to-peak variations 0.5° C | | | |

Notes valid for CC1 – CC2:

- (#) Local measurements repeated on occasion of campaign 1001-2020.
- (\$) Coordinates of mast P7 (APC) were determined on 26.05.2020 using NRCAN PPP
- (*) values based on G1 calib 1001-2020 [RD01]
- (***) values provided by BIPM via Mail 2019-08-07
- (****) PTBM INT DLY were adjusted so that PTBM – PT13 for GPS and Galileo were close to zero for convenience.

Names of files to be used in processing for site PTB
Travelling receiver GZPTBMMJ.DDD, EZPTBMMJ.DDD
Reference receiver GZPT13MJ.DDD, EZPT13MJ.DDD

PTBM operation at FTMC: Receiver LT02

| Laboratory: | | FTMC | |
|--|------------------------|---------------------------------|-----|
| Date and hour of the beginning of measurements: | | 2023-12-04. UTC 09 h. MJD 60282 | |
| Date and hour of the end of measurements: | | 2023-12-08. UTC 11 h. MJD 60286 | |
| Information on the system | | | |
| | Local: | Travelling: | |
| 4-character BIPM code | LT02 | PTBM | |
| Receiver maker and type: | PikTime TTS-5 | Septentrio PolaRx5TR (5.4.0) | |
| Receiver serial number: | SN: 1020 | 3048338 | |
| 1 PPS trigger level /V: | 1.0 | 1.0 | |
| Antenna cable maker and type: | CELLFLEX ¼", LCF14-50J | N-type, LMR400, N-connectors | |
| Phase stabilized cable (Y/N): | Y | N | |
| Length outside the building /m: | ca. 10 m | ca. 10 m | |
| Antenna maker and type: | JAVAD RinGant G3T | Navexperience 3G+C reference | |
| Antenna serial number: | SN: 000656 | S/N RE 0560 | |
| Temperature (if stabilized) /°C | - | - | |
| Measured delays /ns | | | |
| | Local: | Travelling: | |
| Delay from local UTC to receiver 1 PPS-in (X_P) / ns | 86.4 + 112.8 | 9.44 | |
| Delay from 1 PPS-in to internal Reference (if different): (X_O) / ns | 81.05 | N/A | |
| Antenna cable delay: (X_C) / ns | 243 | 264.9 | |
| Splitter delay (if any): | N/A | N/A | |
| Additional cable delay (if any): | N/A | N/A | |
| Data used for the generation of CGGTTS files | | | |
| | LOCAL: | Travelling | |
| <input type="checkbox"/> INT DLY (or X_R+X_S) (GPS) /ns: | N/A | N/A | |
| <input type="checkbox"/> INT DLY (or X_R+X_S) (GALILEO) /ns: | N/A | N/A | |
| <input type="checkbox"/> CAB DLY (or X_C) /ns: | N/A | N/A | |
| <input type="checkbox"/> REF DLY (or X_P+X_O) /ns: | N/A | N/A | |
| <input type="checkbox"/> Coordinates reference frame: | N/A | N/A | |
| X /m: | N/A | | N/A |
| Y /m: | N/A | | N/A |
| Z /m | N/A | | N/A |
| General information | | | |
| <input type="checkbox"/> Rise time of the local UTC pulse: | 5 ns | | |
| <input type="checkbox"/> Is the laboratory air conditioned: | Yes | | |
| Set temperature value and uncertainty: | 23 +/-0.5 °C | | |

PTBM operation at FTMC: Receiver LT03

| Laboratory: | | FTMC | |
|--|------------------------|---------------------------------|-----|
| Date and hour of the beginning of measurements: | | 2023-12-04. UTC 09 h. MJD 60282 | |
| Date and hour of the end of measurements: | | 2023-12-08. UTC 11 h. MJD 60286 | |
| Information on the system | | | |
| | Local: | Travelling: | |
| 4-character BIPM code | LT03 | PTBM | |
| Receiver maker and type: | PikTime TTS-5 | Septentrio PolaRx5TR (5.4.0) | |
| Receiver serial number: | SN: 1029 | 3048338 | |
| 1 PPS trigger level /V: | 1.0 | 1.0 | |
| Antenna cable maker and type: | CELLFLEX ¼", LCF14-50J | N-type, LMR400, N-connectors | |
| Phase stabilized cable (Y/N): | Y | N | |
| Length outside the building /m: | ca. 10 m | ca. 10 m | |
| Antenna maker and type: | JAVAD RinGant G5T | Navexperience 3G+C reference | |
| Antenna serial number: | SN: RA100059 | S/N RE 0560 | |
| Temperature (if stabilized) /°C | - | - | |
| Measured delays /ns | | | |
| | Local: | Travelling: | |
| Delay from local UTC to receiver 1 PPS-in (X_P) / ns | 86.5 | 9.44 | |
| Delay from 1 PPS-in to internal Reference (if different): (X_O) / ns | 87.48 | N/A | |
| Antenna cable delay: (X_C) / ns | 255.9 | 264.9 | |
| Splitter delay (if any): | N/A | N/A | |
| Additional cable delay (if any): | N/A | N/A | |
| Data used for the generation of CGGTTS files | | | |
| | LOCAL: | Travelling | |
| <input type="checkbox"/> INT DLY (or X_R+X_S) (GPS) /ns: | N/A | N/A | |
| <input type="checkbox"/> INT DLY (or X_R+X_S) (GALILEO) /ns: | N/A | N/A | |
| <input type="checkbox"/> CAB DLY (or X_C) /ns: | N/A | N/A | |
| <input type="checkbox"/> REF DLY (or X_P+X_O) /ns: | N/A | N/A | |
| <input type="checkbox"/> Coordinates reference frame: | N/A | N/A | |
| X /m: | N/A | | N/A |
| Y /m: | N/A | | N/A |
| Z /m | N/A | | N/A |
| General information | | | |
| <input type="checkbox"/> Rise time of the local UTC pulse: | 5 ns | | |
| <input type="checkbox"/> Is the laboratory air conditioned: | Yes | | |
| Set temperature value and uncertainty: | 23 +/-0.5 °C | | |

Second common clock measurement at PTB

| | | | | |
|---|--|--|------------------|------------|
| Laboratory: | | PTB | | |
| Date and hour of the beginning of | | 2023-12-16 00:00 UTC (MJD 60294) | | |
| Date and hour of the end of measurements: | | 2023-12-23 23:59 UTC (MJD 60301) | | |
| Information on the system | | | | |
| | Local: | Traveling: | | |
| 4-character BIPM code | PT13 | PTBM | | |
| Receiver maker and type: | PolaRx5TR (5.2.0) | PolaRx5TR (5.3.0) | | |
| Receiver serial number: | S/N 470 1292 | S/N 3048338 | | |
| 1 PPS trigger level /V: | 1 | 1 | | |
| Antenna cable maker and type: Phase stabilized cable (Y/N): | ECOFLEX15 | LMR-400 (N) | | |
| Length outside the building /m: | approx. 25 | 25 | | |
| Antenna maker and type: Antenna serial number: | LEICA AR25 726333, Calib Geo++ 18.08.2015 | Navexperience 3G+C REFERENCE S/N RE 0560 | | |
| Temperature (if stabilized) /°C | | | | |
| Measured delays / ns | | | | |
| | Local: | Traveling: | | |
| Delay from local UTC to receiver 1 PPS-in (X_P) / ns | 9.59 ± 0.1 (#) | 41.13 | | |
| Delay from 1 PPS-in to internal Reference (if different): (X_O) / ns | 46.63 ± 0.1 (#) | Determined automatically by receiver software | | |
| Antenna cable delay: (X_C) / ns | 205.7 ± 0.1 | 264.9 ± 0.5 | | |
| Splitter delay (if any): | N/A | | | |
| Data used for the generation of CGGTTS files | | | | |
| | LOCAL: | Traveling | | |
| <input type="checkbox"/> INT DLY (or X_R+X_S) (GPS) /ns: | 31.6 (P1), 29.3 (P2), 33.6 (C1)(*) | 18.9 (P1) 17.1 (P2) (****) 0.0 (C1) | | |
| <input type="checkbox"/> INT DLY (or X_R+X_S) (GALILEO) /ns: | 33.6 (E1), 33.6 (E5a) (*) | 20.8 (E1), 17.9 (E5a) (****) | | |
| <input type="checkbox"/> CAB DLY (or X_C) /ns: | 205.7 | 264.9 | | |
| <input type="checkbox"/> REF DLY (or X_P+X_O) /ns: | 54.3 | 41.13 | | |
| <input type="checkbox"/> Coordinates reference frame: | ITRF (***) | ITRF (****) | | |
| X /m: | +3844059.86 (***) | Mast P10 | +3844062.56 (\$) | Mast P7 |
| Y /m: | +709661.56 (***) | | +709659.49 (\$) | |
| Z /m | +5023129.87 (***) | | +5023127.88 (\$) | |
| General information | | | | |
| <input type="checkbox"/> Rise time of the local UTC pulse: | 3 ns | | | |
| <input type="checkbox"/> Is the laboratory air conditioned: | Yes | | | |
| Set temperature value and uncertainty: | 23.0 °C, peak-to-peak variations 0.6° C | | | |

Notes valid for CC1 – CC2:

- (#) Local measurements repeated on occasion of campaign 1001-2020.
- (\$) Coordinates of mast P7 (APC) were determined on 26.05.2020 using NRCAN PPP
- (*) values based on G1 CAL_ID 1001-2020 [RD01]]
- (***) values provided by BIPM via Mail 2019-08-07
- (****) PTBM INT DLY were adjusted so that PTBM – PT13 for GPS and Galileo were close to zero for convenience.

Names of files to be used in processing for site PTB

Travelling receiver GZPTBMMJ.DDD, GMPTBMMJ.DDD, EZPTBMMJ.DDD

Reference receiver GZPT13MJ.DDD, GMPT13MJ.DDD, EZPT13MJ.DDD

ANNEX B: PLOTS OF RAW DATA AND TDEV ANALYSIS

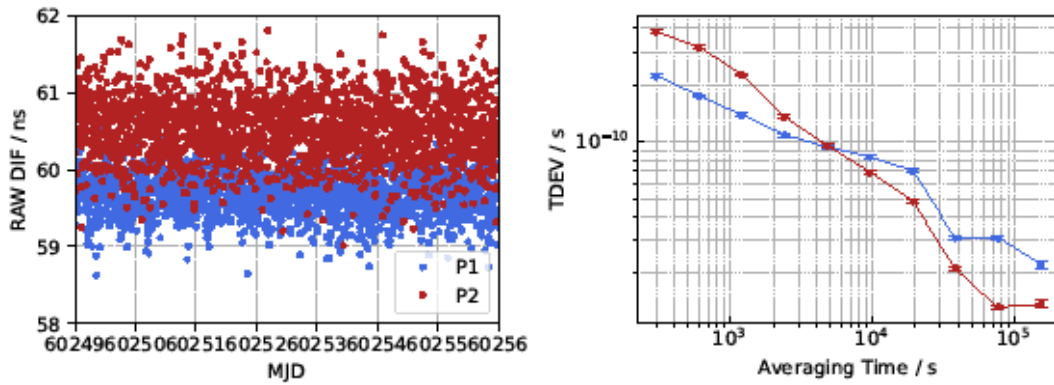


Figure B-1 Left: Raw code differences between T and G for GPS signals during CC1, $\Delta P1$ (blue) and $\Delta P2$ (red) Right: TDEV of the raw code differences between T and G for GPS signals during CC1.

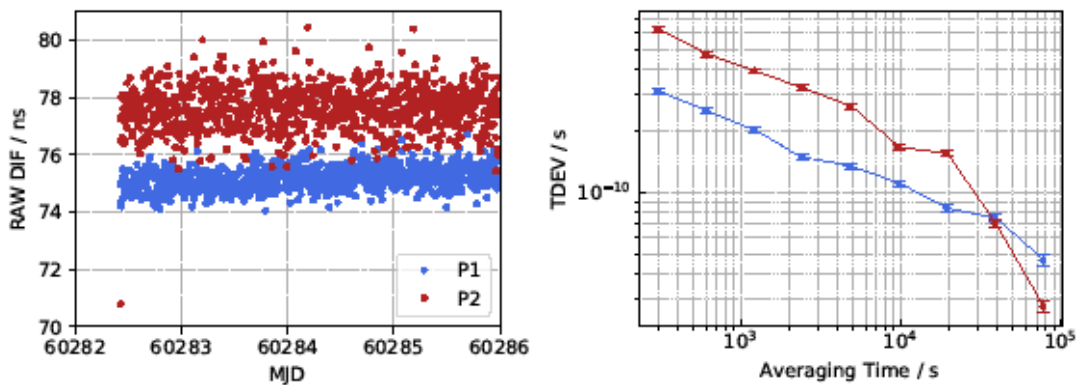


Figure B-2 Left: Raw code differences between T and LT02 for GPS signals, $\Delta P1$ (blue) and $\Delta P2$ (red) Right: TDEV of the raw code differences between T and LT02 for GPS signals.

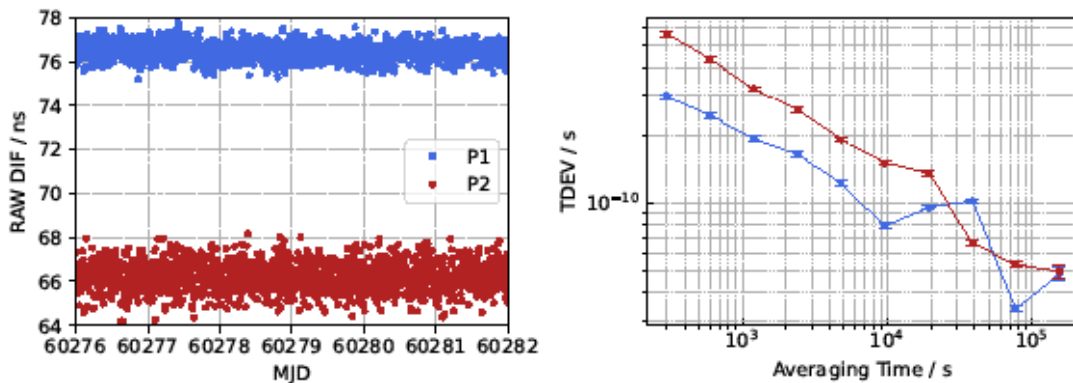


Figure B-3 Left: Raw code differences between T and LT03 for GPS signals, $\Delta P1$ (blue) and $\Delta P2$ (red) Right: TDEV of the raw code differences between T and LT03 for GPS signals.

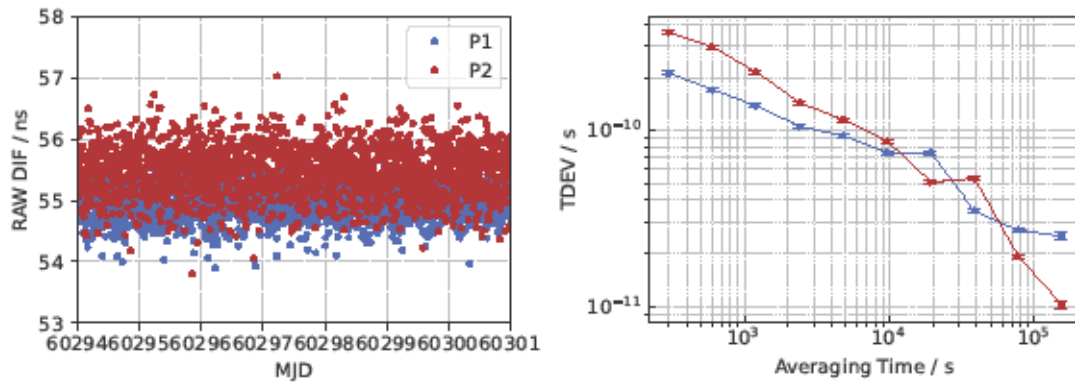


Figure B-4 Left: Raw code differences between T and G for GPS signals during CC2, $\Delta P1$ (blue) and $\Delta P2$ (red) Right: TDEV of the raw code differences between T and G for GPS signals during CC2.

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