Frequency evaluation of UTC(NPL) by NPL-Sr1 for the period MJD 60034 to 60064

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The secondary frequency standard NPL-Sr1 and an optical frequency comb were used to evaluate the frequency of UTC(NPL) over a period of 30 days from MJD 60034 to MJD 60064 (31st March 2023 – 30th April 2023). The Sr optical lattice clock operation covers 88.0% of the total measurement period. The result of the evaluation is reported in table 1 and is made using the CCTF 2021 recommended frequency value for the $5s^2$ 1S_0 – 5s5p 3P_0 unperturbed optical transition in ^{87}Sr : 429 228 004 229 872.99 Hz with a relative standard uncertainty of $u_{\rm Srep} = 1.9 \times 10^{-16}$ [1].

Period of	y(UTC(NPL)-	$u_{\rm A}$	u_{B}	$u_{\rm A/Lab}$	$u_{\rm B/Lab}$	u_{Srep}	Uptime
estimation	$NPL-Sr1) /10^{-16}$	$/10^{-16}$	$/10^{-16}$	$/10^{-16}$	$/10^{-16}$	$/10^{-16}$	
MJD 60034-60064	-0.57	0.003	0.102	1.73	1.29	1.9	88.0%

Table 1: Results of the evaluation of UTC(NPL) by NPL-Sr1.

1 Measurement configuration

NPL-Sr1 was operated as described in reference [2], with the exception of some changes described in section 2 below. The 698 nm clock laser was pre-stabilized to a local reference cavity and then phase-locked via a fibre-based optical frequency comb to another more stable laser at 1064 nm. A feedback loop acting on an acousto-optic modulator (AOM) kept the clock laser frequency in resonance with the ⁸⁷Sr clock transition.

Following a change in the reference maser for UTC(NPL) in January 2021, and a subsequent redistribution of reference frequency signals within NPL in February 2021, the optical frequency comb was no longer referenced to UTC(NPL), but instead to a separate maser reference HM6.

The frequency ratio between the ⁸⁷Sr clock transition and HM6 was calculated from the comb measurements of the 698 nm ultrastable laser and the AOM frequency corrections. The frequency ratio was determined as the midpoint of a weighted linear fit to the NPL-Sr1/HM6 ratio data. The time offset between HM6 and UTC(NPL) was continually measured by an SR620 time interval logger. By taking the derivative of this time offset we determined the mean frequency difference between the two signals over the evaluation period. This was then combined with the frequency comb measurements to obtain the frequency ratio between the ⁸⁷Sr clock transition and UTC(NPL). HM6 was not steered during this evaluation period.

Systematic effect	Correction / 10^{-18}	Uncertainty / 10^{-18}	
BBR chamber	4966.0	9.3	
BBR oven	0.5	0.5	
Quadratic Zeeman	233.7	0.3	
Lattice	-5.0	2.2	
Collisions	0.0	2.0	
Background gas	6.4	1.0	
DC Stark	0.016	0.016	
Probe Stark	0.0	1.0	
Servo Error	0.0	0.0	
Total Correction	5201.6	9.9	
Gravitational redshift	-1215.0	2.7	
Total including gravitational redshift	3986.6	10.2	

Table 2: Uncertainty budget of the NPL-Sr1 lattice clock for this evaluation period. Reported uncertainties correspond to 68% confidence intervals.

2 NPL-Sr1 evaluation

Type A uncertainty

The type A uncertainty u_A is the statistical contribution from the frequency instability of NPL-Sr1. This was estimated based on a white frequency noise component of $4.5 \times 10^{-16}/\sqrt{\tau}$, extrapolated to the duration of the evaluation period.

This is an improvement compared to the earlier reports covering the periods MJD 58659–58679 $(5 \times 10^{-16}/\sqrt{\tau})$, MJD 58454–58459 $(8 \times 10^{-16}/\sqrt{\tau})$ and MJD 57904–57919 and MJD 57929–57934 $(2 \times 10^{-15}/\sqrt{\tau})$. The improvement is a direct result of improvements made to the 1064 nm laser to which the 698 nm clock laser is stabilised. The stability was evaluated by interleaved measurements.

Type B uncertainty

The type B uncertainty u_B is the sum in quadrature of the systematic uncertainty of NPL-Sr1 and the uncertainty of the gravitational redshift relative to the conventionally adopted reference potential $W_0 = 62~636~856.0~{\rm m}^2{\rm s}^{-2}$.

The systematic frequency corrections and uncertainty budget for NPL-Sr1 for the period of this report are given in table 2. The geopotential value for NPL-Sr1 is taken from [3].

Changes to the uncertainty evaluation presented in reference [2] are described below.

$Blackbody\ radiation$

In this report we use an updated dynamic correction coefficient for blackbody radiation, reported in reference [4]. This leads to an increase of 4×10^{-18} in the total BBR correction for our operational conditions close to 300 K, compared to the value obtained using the previous coefficient.

Quadratic Zeeman

For this evaluation, we returned to using a stretched state splitting similar to that used in reference [2], following an increase for the reports covering the periods MJD 58454–58459 and MJD 58659–

58679. However, we continue to use the updated value for the quadratic Zeeman shift coefficient of $-2.456(3) \times 10^{-7} \text{ Hz}^{-1}$ [5].

Background Gas

As for the previous evaluations, we use an updated coefficient for the background gas collisional shift of $(-3.0 \pm 0.3) \times 10^{-17}/\tau$, where τ is the 1/e vacuum-limited trap lifetime [6]. Assuming hydrogen is the dominant gas in our system we arrive at a shift of $(-6.4 \pm 1.0) \times 10^{-18}$ based on a lattice trapped lifetime measurement of 4.7 s (re-evaluated recently after breaking vacuum for replacement of the Zeeman slowing beam viewport). Unlike previous reports where the gas composition was unknown, an evaluation of the residual gas content of the vacuum shows hydrogen as dominant and so we assign a total uncertainty for the shift of 1.0×10^{-18} which is a combination of the coefficient and vacuum lifetime measurement uncertainties.

Collisions

In August 2018, a lattice enhancement cavity was implemented on NPL-Sr1. As a result, the trapping waist is considerably larger than in reference [2] (153 μ m compared to 65 μ m). A re-evaluation of the cold collisional shift was completed for the reported evaluation period by comparing operation at high and low atom number. The shift was determined to be consistent with zero within an uncertainty of 2.0×10^{-18} for nominal operating conditions.

Lattice

A full re-evaluation of the lattice shift was completed for the reported evaluation period and followed the approach set out in reference [2]. Updated coefficients for the hyper- and E2-M1 multipolar polarisability terms were used as described in ref [7]; using a weighted mean for the hyper-polarisability term and the multipolar polarisability coefficient reported in ref [8]. The total scalar/tensor shift was determined to be $(-2.2\pm1.8)\times10^{-18}$ and the higher order hyper- and multipolar polarisability shifts as $(-1.5\pm0.4)\times10^{-18}$ and $(8.8\pm1.2)\times10^{-18}$ respectively, giving a total lattice light shift of $(5.0\pm2.2)\times10^{-18}$.

3 Frequency comparison

Type A uncertainty

The uncertainty $u_{A/Lab}$ arises mainly from the dead time in the comparison between HM6 and NPL-Sr1, and includes both a deterministic correction due to maser drift and a stochastic contribution (table 3).

Contribution	Uncertainty / 10^{-18}		
$u_{\rm A/Lab}[{ m Deterministic}]$	2		
$u_{\rm A/Lab}[{ m Stochastic}]$	173		
$u_{\rm A/Lab}[{\rm HM6\text{-}UTC(NPL)}]$	11		
$u_{ m A/Lab}[{ m Total}]$	173		

Table 3: A breakdown of the uncertainties included in $u_{A/Lab}$.

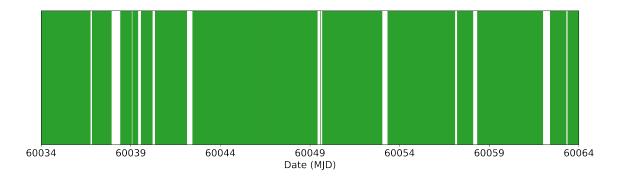


Figure 1: Uptime of NPL-Sr1 over the evaluation period (green regions).

The stochastic contribution was estimated by a method described in reference [9]. This involves a Monte-Carlo approach where the frequency noise of HM6 is simulated and a value calculated for the offset between the mean frequency during the uptime periods and the mean frequency during the whole evaluation period. The simulation was repeated 1000 times, with the standard deviation of the offsets providing an estimate for the frequency uncertainty arising from the dead times in the operation of NPL-Sr1.

The maser noise model used comprised white phase noise of $2.50 \times 10^{-13}/\tau$, white frequency noise of $4.90 \times 10^{-14}/\sqrt{\tau}$, a flicker frequency floor of 1.25×10^{-15} and a random-walk frequency component of $2.55 \times 10^{-19}\sqrt{\tau}$. In addition, maser HM6 exhibits periodic frequency fluctuations that were estimated as an additional noise process proportional to the sum of four sinusoids in the simulated noise, with amplitudes 6.0×10^{-15} , 2.5×10^{-15} , 3.0×10^{-15} and 3.0×10^{-15} and periods 3×10^3 s, 3×10^4 s, 8.64×10^4 s and 1.728×10^5 s respectively. These values were derived from measurements of HM6 by NPL-Sr1 and our caesium fountain primary frequency standard NPL-CsF2 during the evaluation period.

For this evaluation period, NPL-Sr1 had an uptime of 88.0%, distributed as shown in figure 1. The SR620 time interval logger that links HM6 to UTC(NPL) introduces an additional contribution to $u_{\rm A/Lab}$, which is computed from the statistical spread of the time interval measurements.

Type B uncertainty

The most significant contribution to the uncertainty $u_{\rm B/Lab}$ is the distribution of the 10 MHz signal from HM6 to the frequency comb laboratory, and the subsequent synthesis in that laboratory of an 8 GHz signal against which the repetition rate of the frequency comb was measured. Potential phase fluctuations were monitored using a loop-back comparison as described in reference [2], and their contribution to the uncertainty estimated from the instability of these fluctuations over the evaluation period.

The SR620 time interval logger that links HM6 to UTC(NPL) also contributes to $u_{\rm B/Lab}$. This contribution is estimated based on the specification of the instrument.

References

[1] Consultative Committee for Time and Frequency (CCTF), "Recommendation PSFS-2 from the 22nd meeting (session II – online)," (2022).

Contribution	Uncertainty / 10^{-18}		
$u_{\rm B/Lab}[{\rm Distribution}]$	126		
$u_{\rm B/Lab}[{\rm HM6\text{-}UTC(NPL)}]$	27		
$u_{ m B/Lab}[{ m Total}]$	129		

Table 4: A breakdown of the uncertainties included in $u_{\rm B/Lab}$.

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